

Design Kit

NJM2377–Boost DC/DC Converter

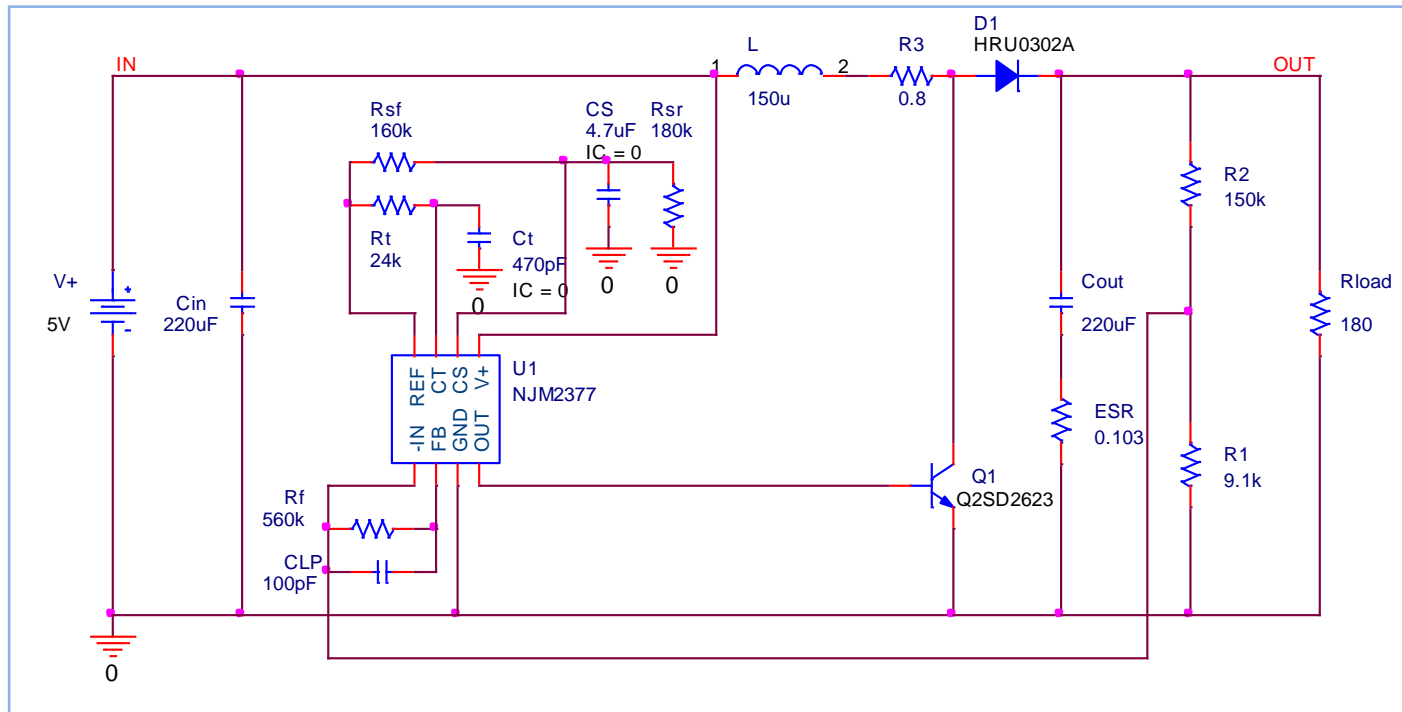
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1. NJM2377 – Boost DC/DC Converter Circuit

5V to 9V at 50mA Boost DC/DC Converter ($f_{OSC}=150kHz$, $V_{ripple}=30mV_{p-p}$)

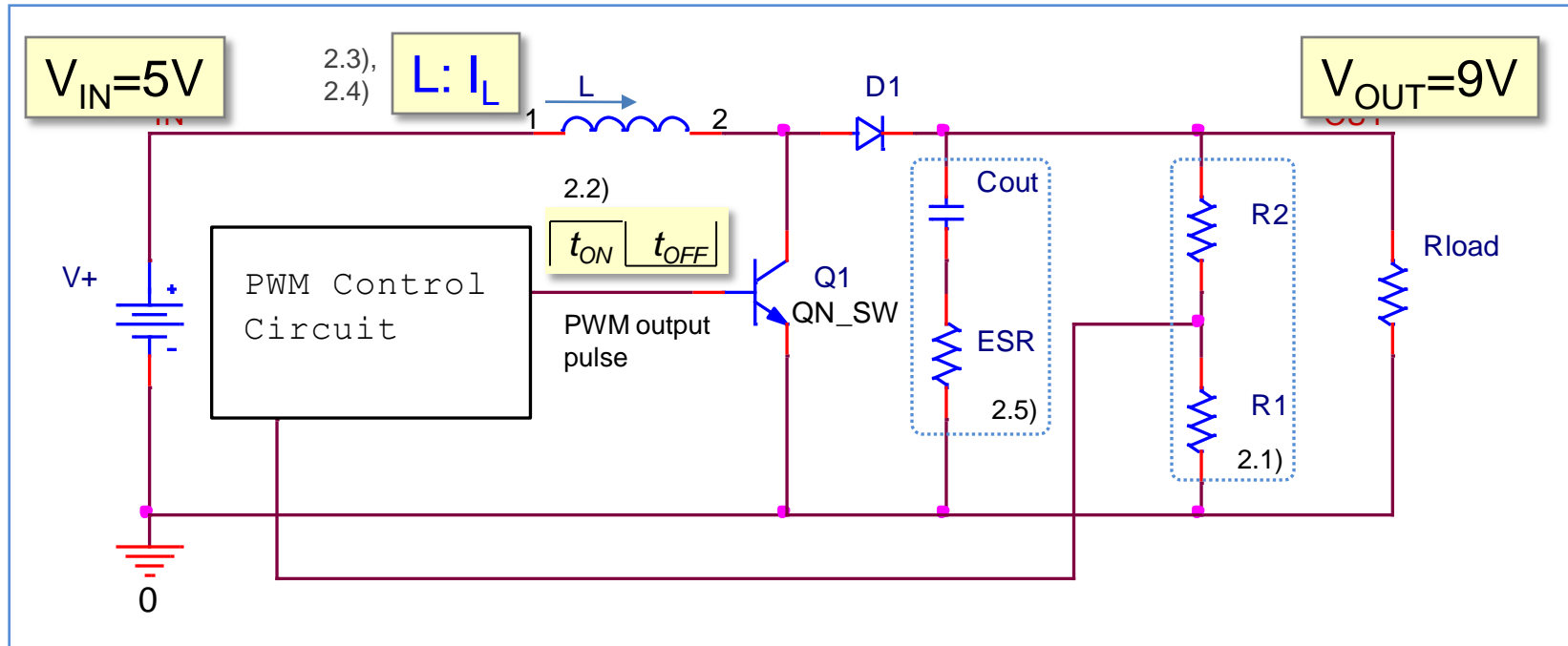


U1: New Japan Radio NJM2377 Control IC

Q1: Panasonic 2SD2623 NPN

D1: Renesas HRU0302A Schottky Barrier Diode

2. PWM – Boost DC/DC Converter Basic Operation and Design



- V_{OUT} is monitored by R_1 and R_2 then compared to reference voltage V_B in NJM2377.
- Error voltage is pulse width modulated with sawtooth waveform.
- PWM output pulse width is proportional to the error level. This signal will control the switch ON/OFF (t_{ON}/t_{OFF}).
- Therefore V_{OUT} , which is proportional to t_{ON}/t_{OFF} , is controlled to the desired voltage.

2.1 Boost DC/DC Converter – V_{OUT}

- V_{OUT} is determined by R1 and R2, without considering I(IN-) of NJM2377 V_{OUT} is calculated as below.

$$\begin{aligned}V_{OUT} &= \left(\frac{R2}{R1} + 1 \right) \times V_{REF} \\ &= \left(\frac{150k}{9.1k} + 1 \right) \times 0.52 = 9.09V\end{aligned}$$

- For $V_{OUT}=9V$, $R1=9.1k\Omega$, $R2=150k\Omega$ are selected.

2.2 Boost DC/DC Converter – t_{ON}/t_{OFF}

- If the circuit works in continuous conduction mode (CCM), output voltage (V_{OUT}) and ON/OFF time (t_{ON}/t_{OFF}) follow the equation below.

$$V_{OUT} = \left(\frac{t_{ON} + t_{OFF}}{t_{OFF}} \right) \times V_{IN}$$

then

$$t_{ON} = \frac{V_{OUT} - V_{IN}}{V_{OUT} \times f_{OSC}}$$

- From $V_{IN}=5V$, $V_{OUT}=9V$ and $f_{OSC}=150kHz$, these result as t_{ON}/t_{OFF} are $t_{ON}=2.96\mu s$, $t_{OFF}=3.71\mu s$, and duty=45%.

2.3 Boost DC/DC Converter – Inductor Selection

- L_{MIN} value for the converter to work in continuous conduction mode (CCM), is calculated as below.

$$L_{MIN} = \frac{V_{IN}^2}{2 \times V_{OUT} \times I_{OUT}} \times t_{ON}$$

- From $V_{IN}=5V$, $V_{OUT}=9V$, $I_{OUT}=50mA$ and $t_{ON}=2.96\mu s$, these result as $L_{MIN}=82.2\mu H$.

$$L_{MIN} < L < 2 \times L_{MIN}$$

- A larger value will be used to increase the available output current, but limit it to around twice the L_{MIN} value. $L=150\mu H$ is selected.

2.4 Boost DC/DC Converter – Inductor Peak Current

- $I_{L,PK}$ is calculated as below.

$$I_{L,PK} = \frac{V_{OUT} \times I_{OUT}}{V_{IN}} + \frac{V_{IN}}{2 \times L} \times t_{ON}$$

$$= \frac{9 \times 0.05}{5} + \frac{5}{2 \times 150 \mu} \times 2.96 \mu = 140 \text{mA}$$

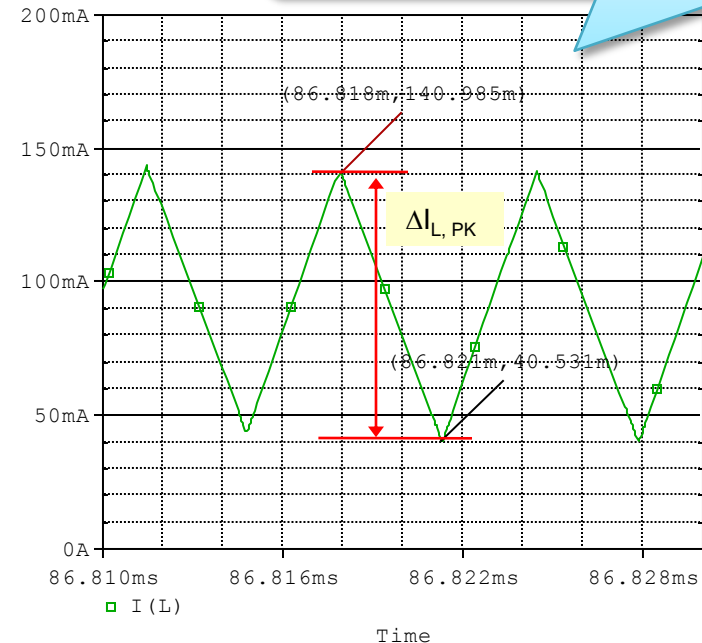
- And the current ripple - $\Delta I_{L,PK}$ is calculated as below

$$\Delta I_{L,PK} = \frac{V_{IN}}{L} \times t_{ON}$$

$$= \frac{5}{150 \mu} \times 2.96 \mu = 99 \text{mA}$$

- PSpice is used to verify the circuit design.

• Add trace I(L)
• Zoom to check the peak value.



- $I_{L,PK} = 140.985 \text{mA}$ and $\Delta I_{L,PK} = 140.985 \text{m} - 40.531 \text{m} = 100.454 \text{mA}$

2.5 Boost DC/DC Converter – C_{OUT} Selection

- C_{OUT} is determined from the V_{ripple} Spec (30mV_{p-p}).
- If C_{OUT} >> I_{OUT}·ton/V_{ripple} (50m·2.96μ/30m=4.933μF), V_{ripple} will mainly be caused by ESR.

$$ESR < \frac{V_{ripple(p-p)}}{\Delta I_L}$$

$$= \frac{30m}{99m} = 103m\Omega$$

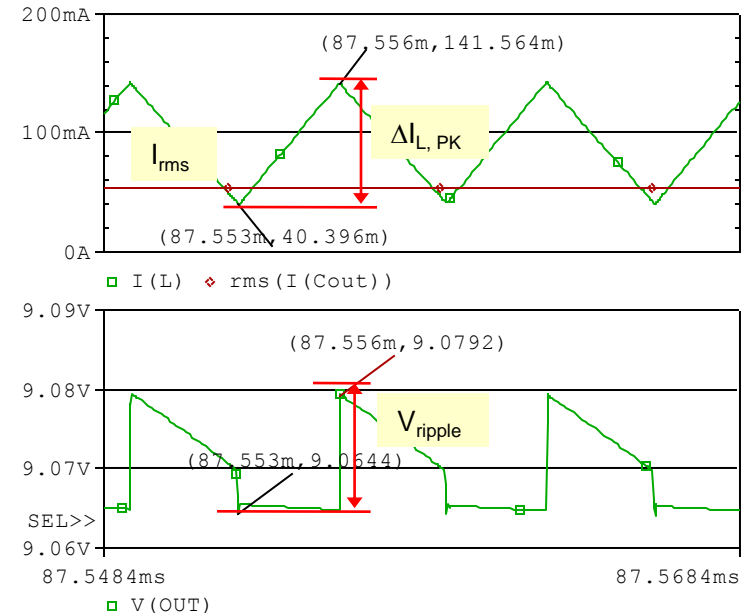
- Select the capacitor that can handle the ripple current I_{rms}.

$$I_{rms} = \frac{\Delta I_L}{2\sqrt{3}} \times \frac{ton}{t}$$

$$= \frac{99m}{2\sqrt{3}} \times \frac{2.96\mu}{6.67\mu} = 13mArms$$

- C_{OUT}=220μF, ESR=103mΩ is selected.

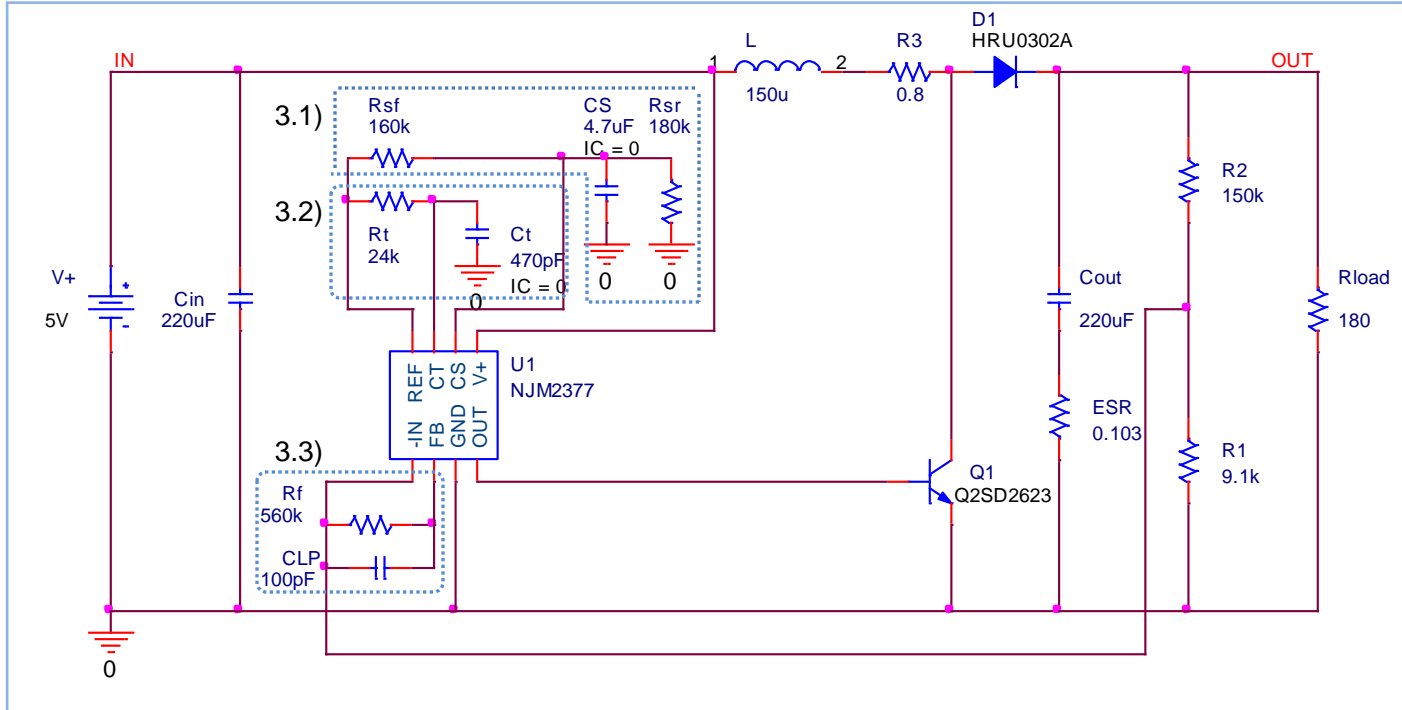
- PSpice is used to verify the circuit design.



- ΔI_{L,PK}=101.168mA, ton=3μs.
 - V_{ripple} = 14.8mV_{p-p}
 - I_{rms}* = 53.856mArms.
- ※ I_{rms} is larger than calculated value due to feedback loop response ripple current.

3. NJM2377 – Application Circuit Configuration

5V to 9V at 50mA Boost DC/DC Converter ($f_{OSC}=150kHz$)



U1: New Japan Radio NJM2377 Control IC

Q1: Panasonic 2SD2623 NPN

D1: Renesas HRU0302A Schottky Barrier Diode

3.1 NJM2377 – Soft Start Time Setting

NJM2377 soft-start time is determined by Rsr, CS and Rsf

- First, calculate Rsr by $Rsr > V_{THLA(max.)} / I_{CHG(min.)}$
(1.8V/10μA=180kΩ)
- During steady state operation, I(CS)=I_{BCS}=250ns. Maximum duty cycle is determined by V(CS). Set V(CS)=V_{THCS(max.)}=0.8V, Rsf is calculated by

$$V_{THCS(max.)} = \frac{Rsr}{Rsr + Rsf} \times V_{REF}$$

$$0.8 = \frac{180k}{180k + Rsf} \times 1.5$$

$$Rsf = 160k\Omega$$

- Soft-start time or t_{duty(max.)} is time needed for V(CS) to reach V_{THCS(max.)} by charging capacitor Cs.
- CS is charged by current Ics, calculated by:

$$I_{CS} = \frac{V_{REF}}{Rsr + Rsf}$$

$$= \frac{1.5}{180k + 160k} = 4.41\mu A$$

then

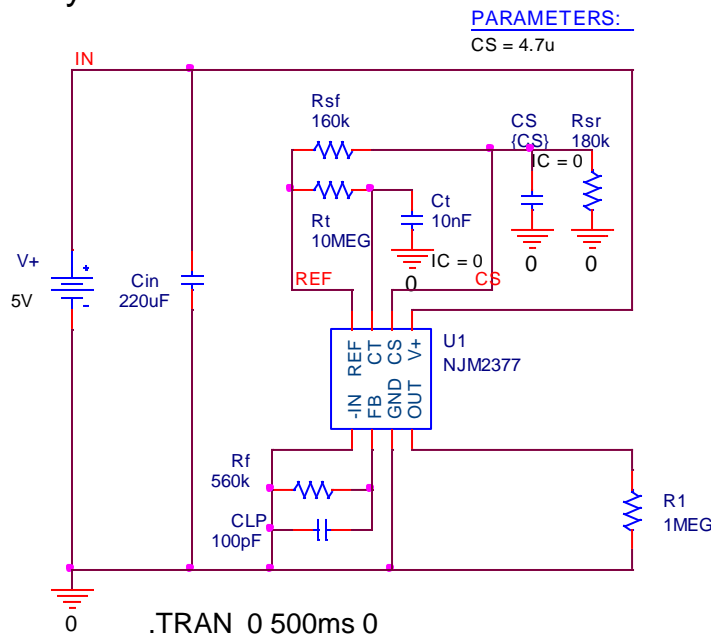
$$t_{duty(max.)} = \frac{V_{THCS(max.)} \times Cs}{I_{CS} + I_{CHG}}$$

$$= \frac{0.8 \times 4.7\mu}{4.41\mu + 30\mu} = 109ms$$

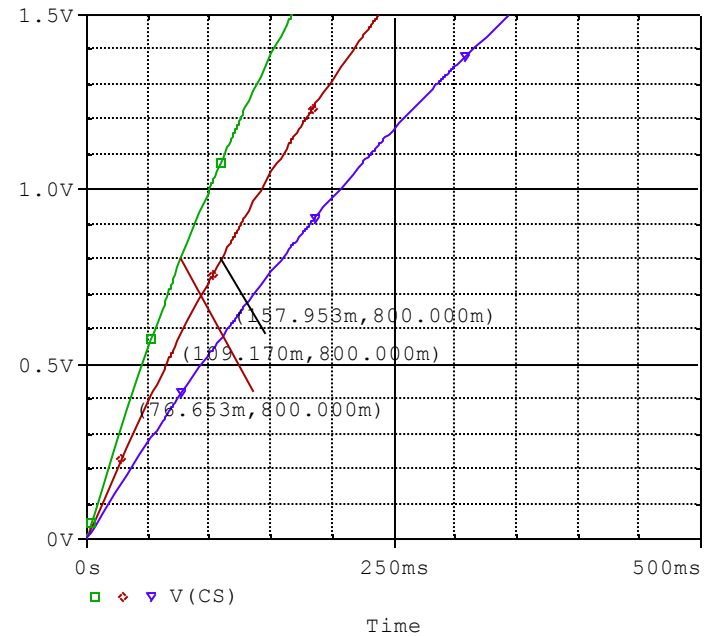
3.1 NJM2377 – Soft Start Time Setting (Simulation)

NJM2377 soft-start time is determined by Rsr, Rsf and CS

- Select Rsr, Rsf, and CS then check $t_{duty(max.)}$ by simulation.



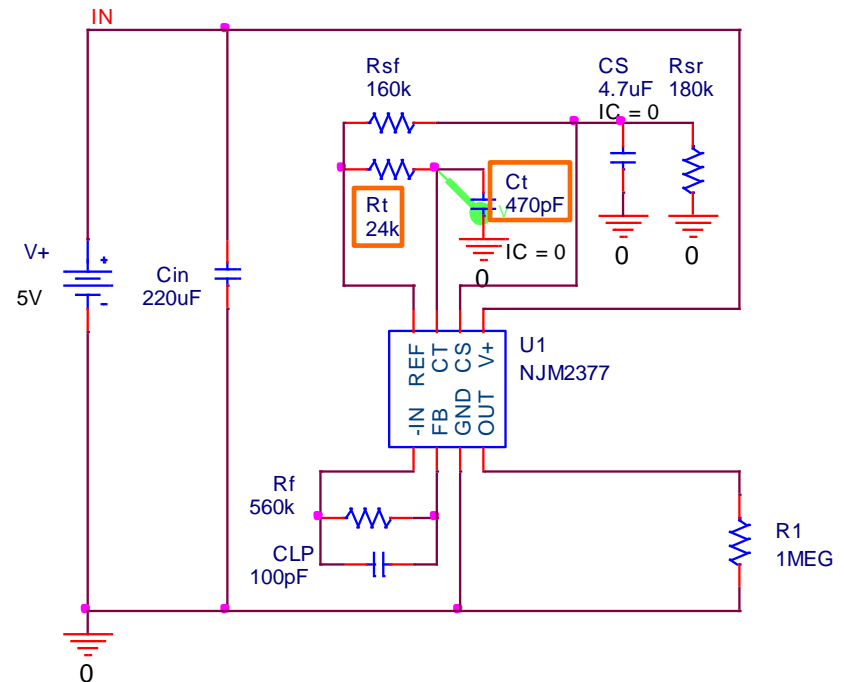
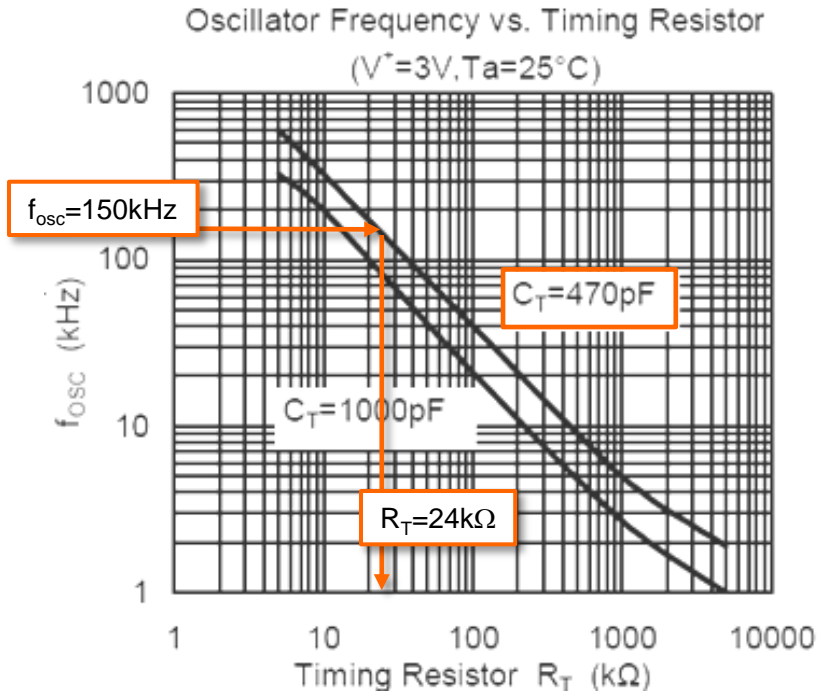
- $t_{duty(max.)} = 109.170ms$ for CS=4.7uF



- $t_{duty(max.)} = 76.653ms$ for CS=3.3uF and $t_{duty(max.)} = 157.953ms$ for CS=6.8uF.

3.2 NJM2377 – Oscillation Frequency Setting

NJM2377 oscillation frequency f_{OSC} is determined by C_T and R_T



- $C_T = 470pF$ and $R_T = 24k\Omega$ to set an oscillation frequency to be 150kHz.

3.3 Error Amp Feed Back Loop Setting

Error Amp Feed Back Loop is determined by R1, R2, Rf and CLP

- For F.B loop gain $G > 100$, Rf is calculated as:

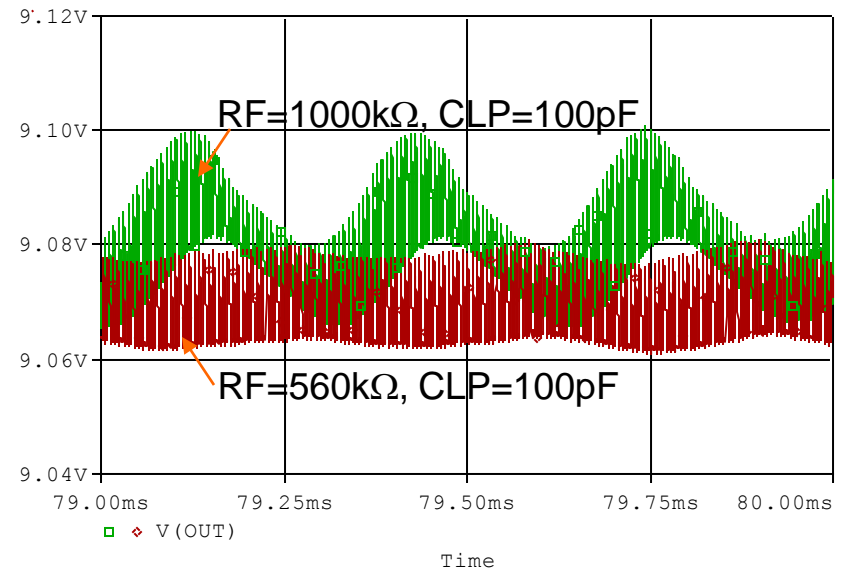
$$G = \frac{R_f}{R1 // R2}$$

$$= \frac{1,000k}{150k // 9.1k} = 177$$

Rf = 1000k

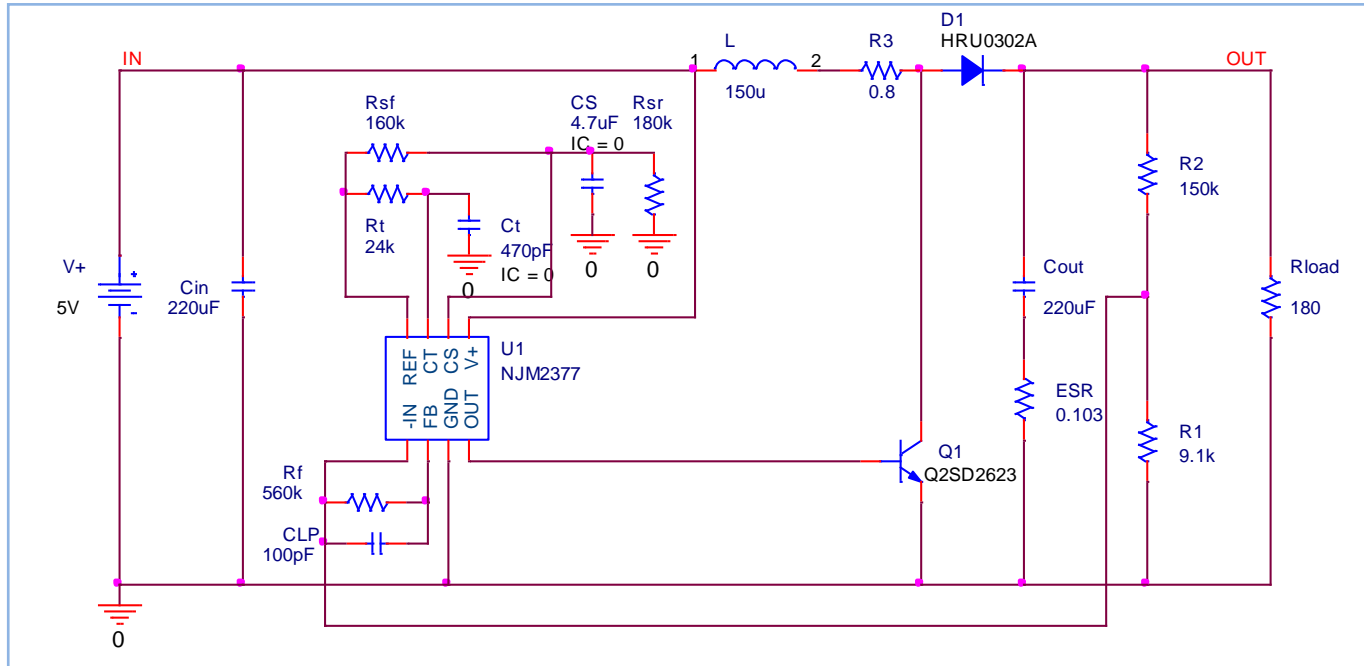
- CLP is suggested to use value between **100pF~1,000pF**
- Inappropriate F.B loop design can cause an oscillation. PSpice is used to verify the ripple voltage vs. Rf and CLP values.

- Simulation result shows V_{ripple} of the circuit with $R_F=1000k\Omega$ compare to the circuit with $R_F=560k\Omega$.



- Changing R_F to be $560k\Omega$ can reduce V_{ripple} from $34mV_{p-p}$ to less than $20mV_{p-p}$.

4. Performance Characteristics



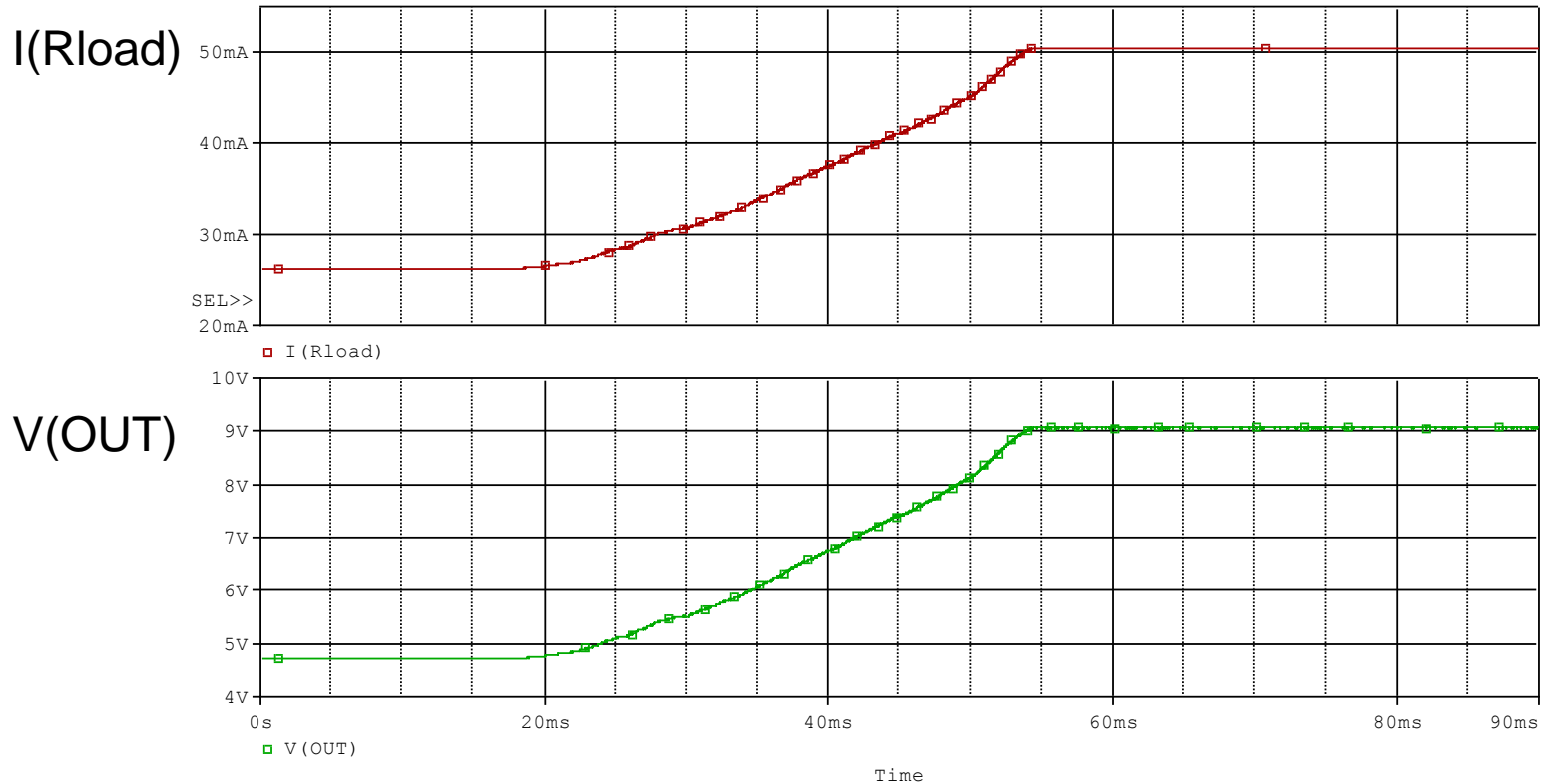
- $V_{IN}=5V$
- $V_{OUT}=9V$
- $I_{OUT}=50mA$
- $V_{ripple(P-P)}$ = less than 30mV
- Efficiency = 75% at $I_{OUT}=50mA$

U1: New Japan Radio NJM2377 Control IC

Q1: Panasonic 2SD2623 NPN

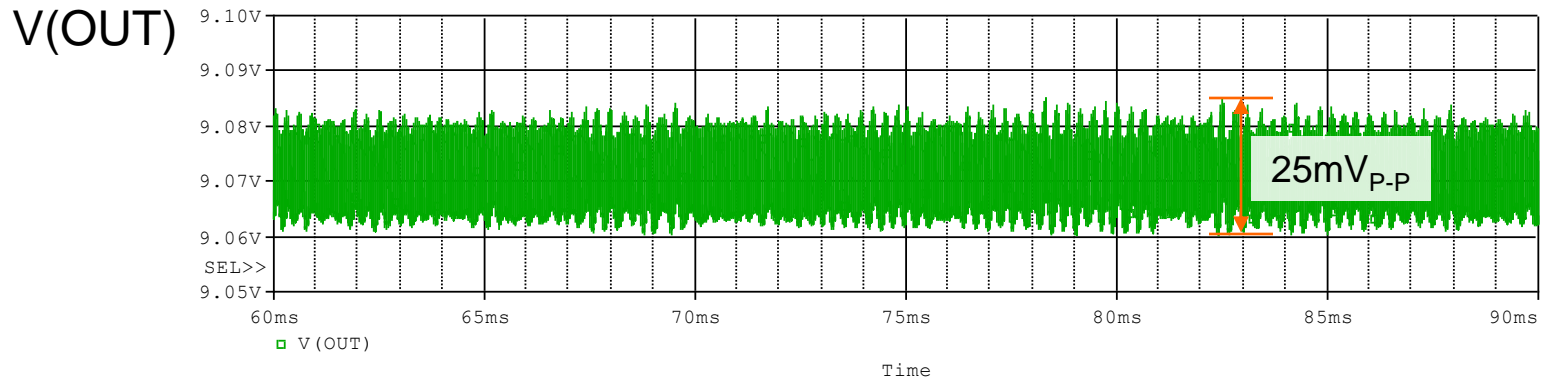
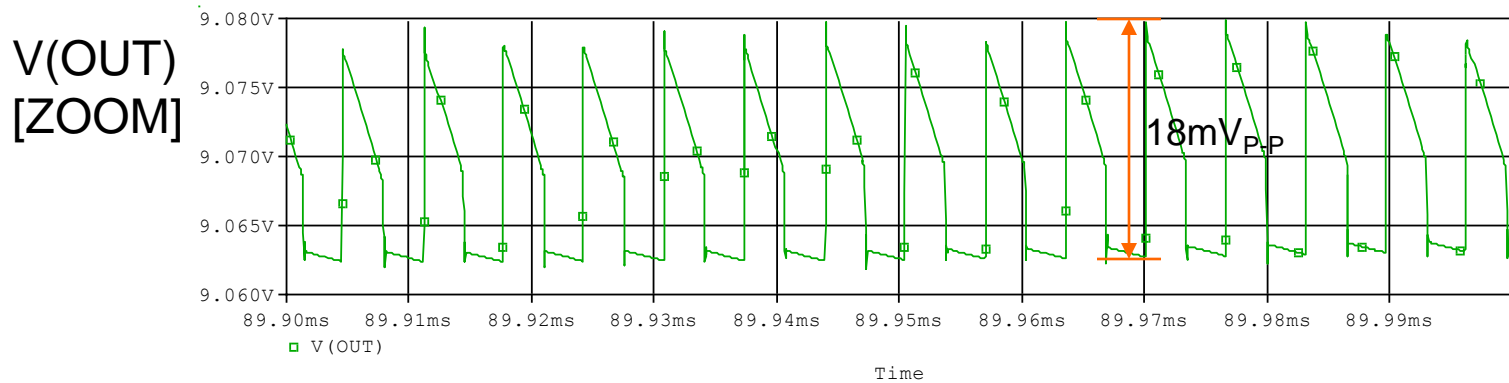
D1: Renesas HRU0302A Schottky Barrier Diode

4.1 Output Start-Up Voltage and Current



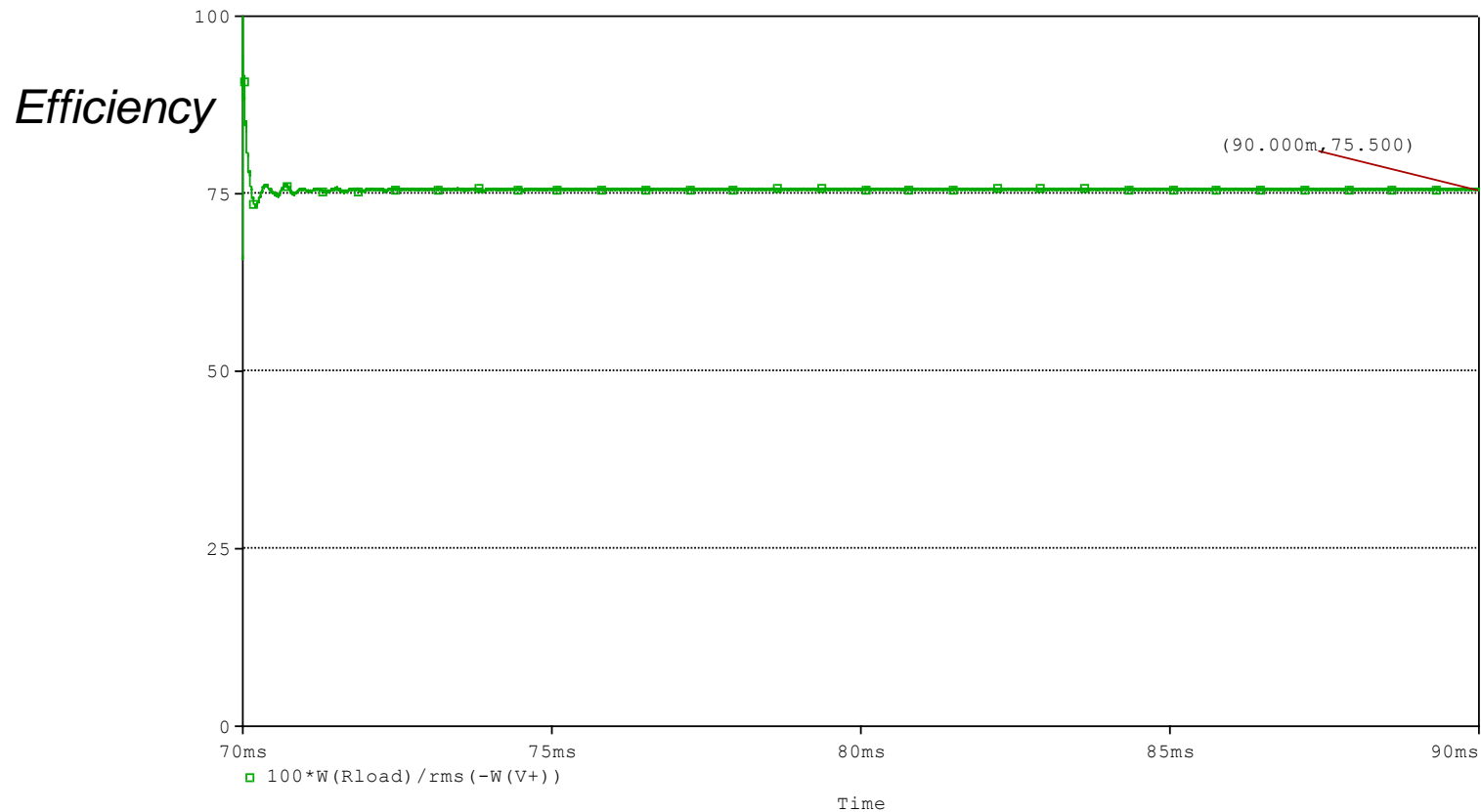
- Simulation result shows output start-up time of the circuit. This circuit needs 55ms to reach steady state.

4.2 Output Ripple Voltage



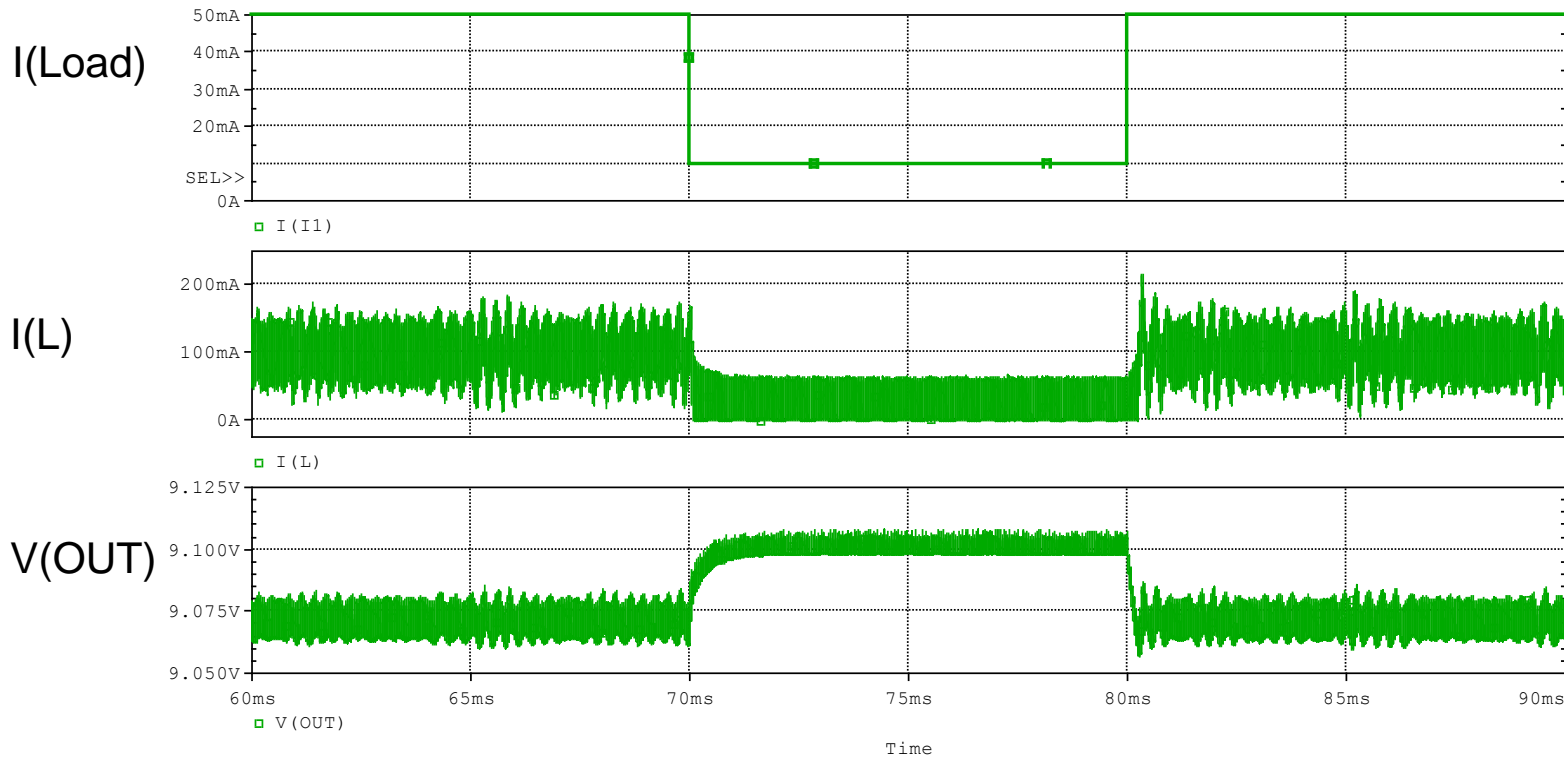
- Simulation result shows output ripple voltage caused by switching(18mV_{P-P}) and F.B loop oscillation(25mV_{P-P}).

4.3 Efficiency



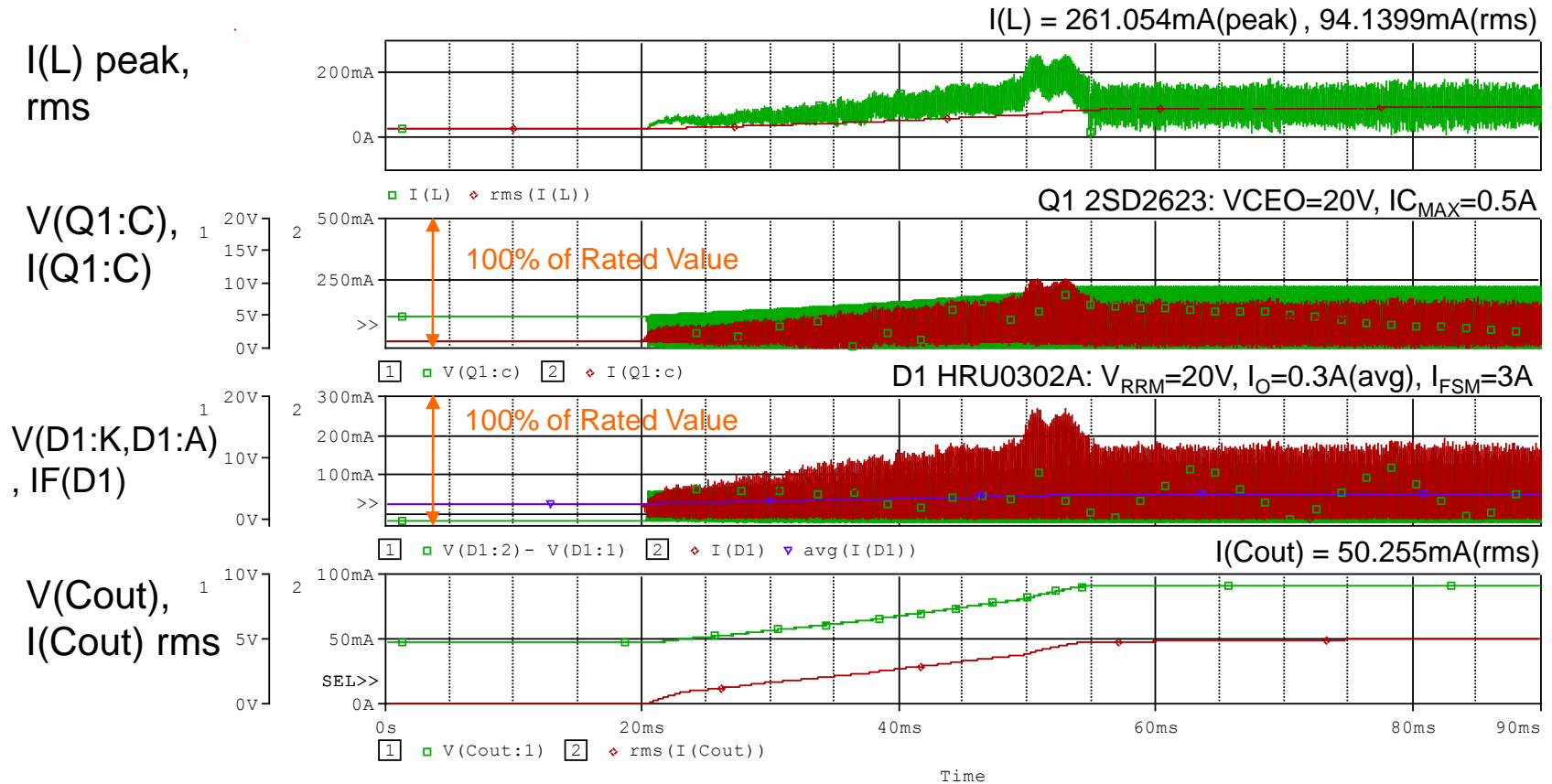
- Efficiency of the converter at load $I_{OUT}=50mA$ is 75.5%.

4.4 Step-Load Response



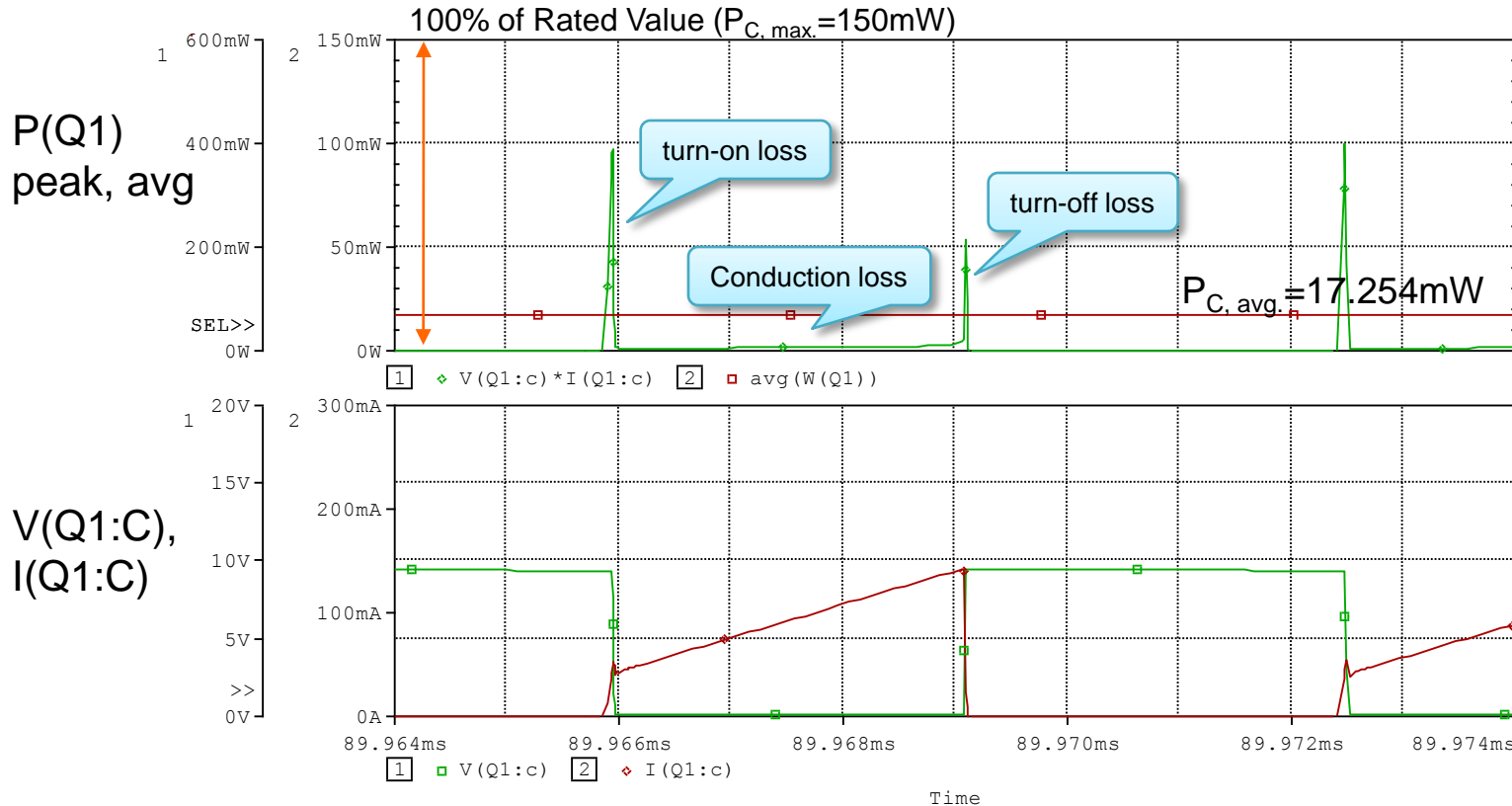
- Simulation result shows the transient response of the circuit, when load currents are 50mA to 10mA to 50mA steps .

5. Voltage and Current Simulation Result



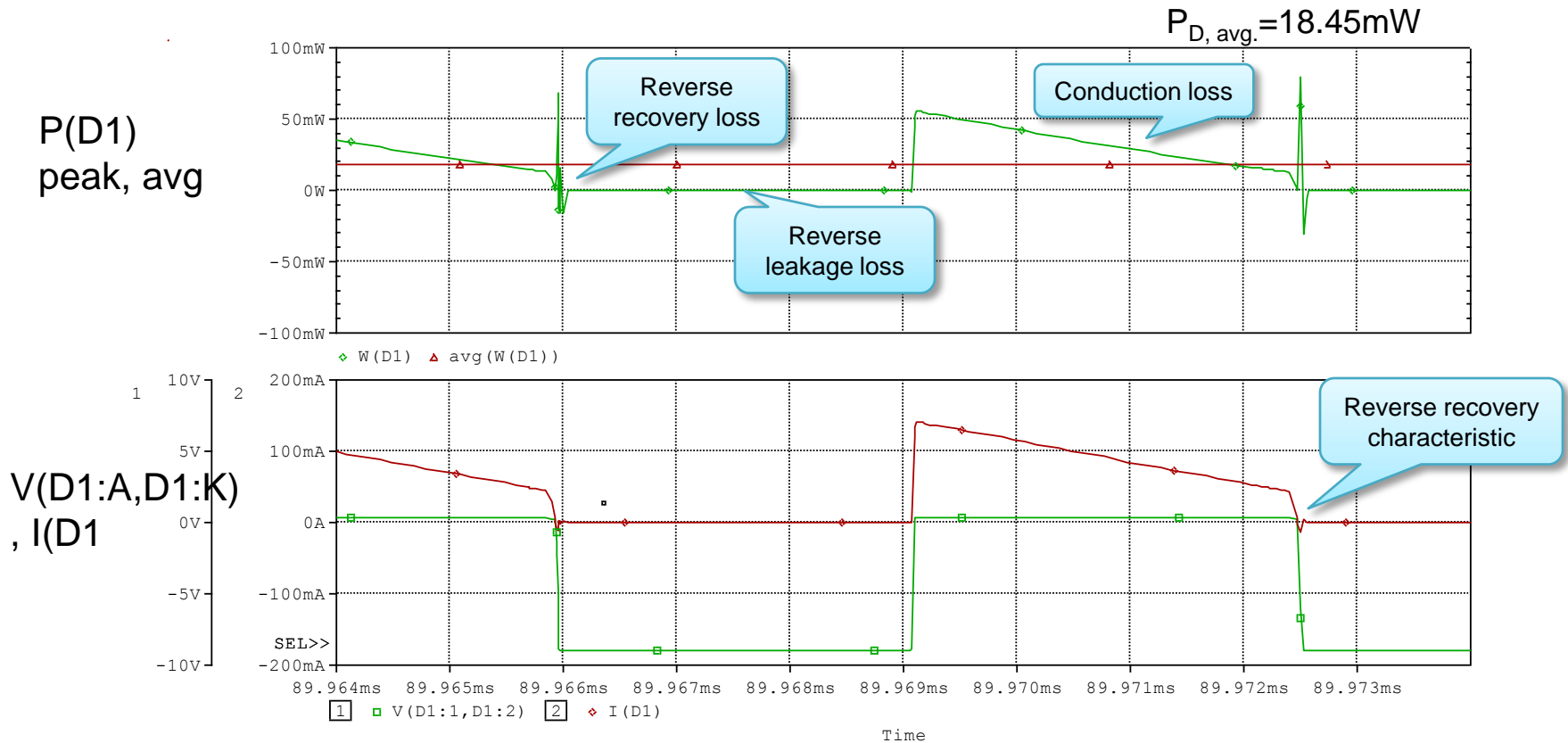
- Simulation result shows voltage and current of the devices.
- Select L and Cout that can handle their I_{rms} value.
- The absolute maximum value of Q1 and D1 are compared to simulation result for stress analysis.

6.1 Bipolar Junction Transistor Losses



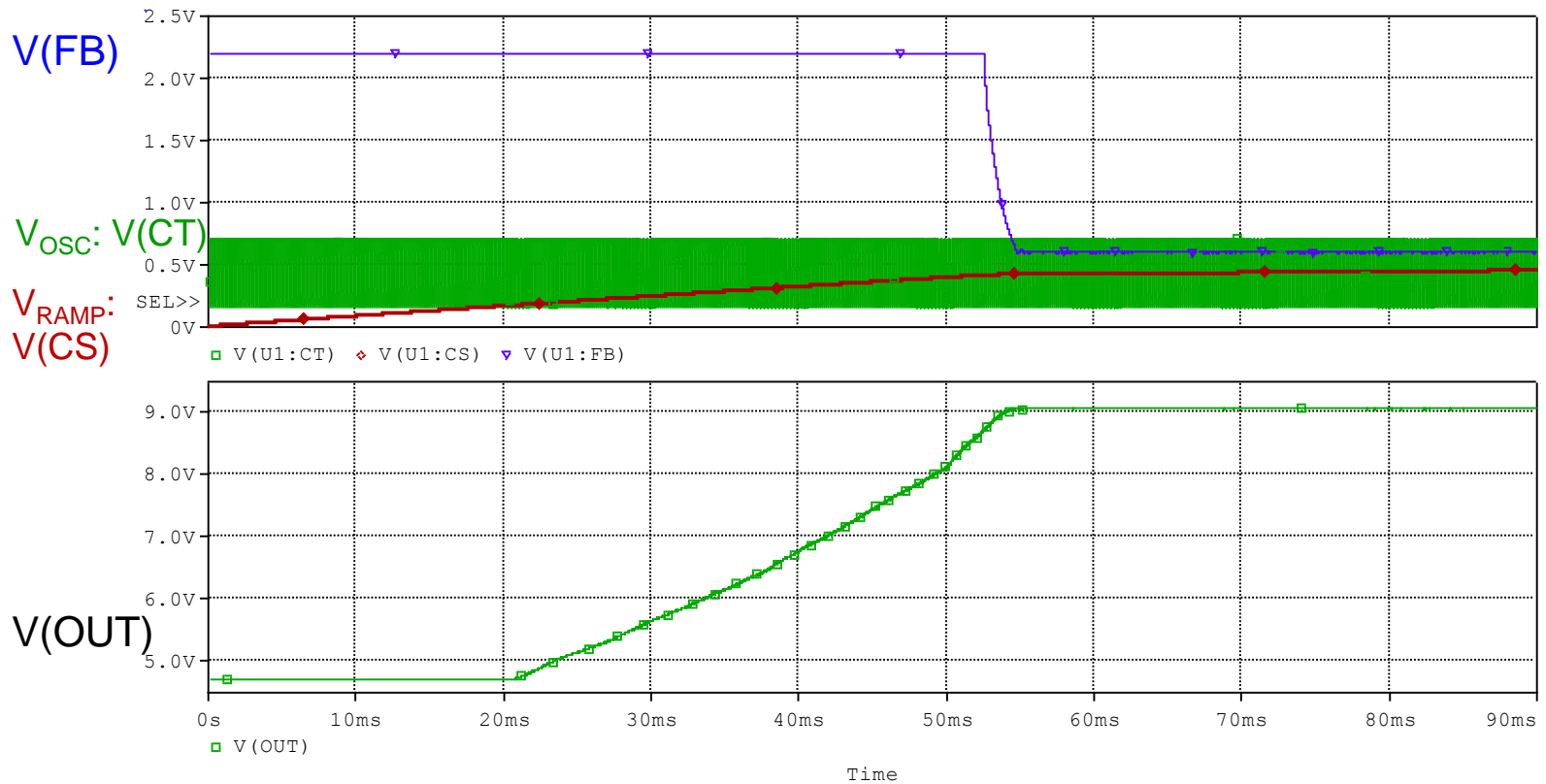
- Simulation result shows waveforms of I_C and V_{CE} of transistor Q1. Loss in peak and average values are also shown.

6.2 Schottky Barrier Diode Losses



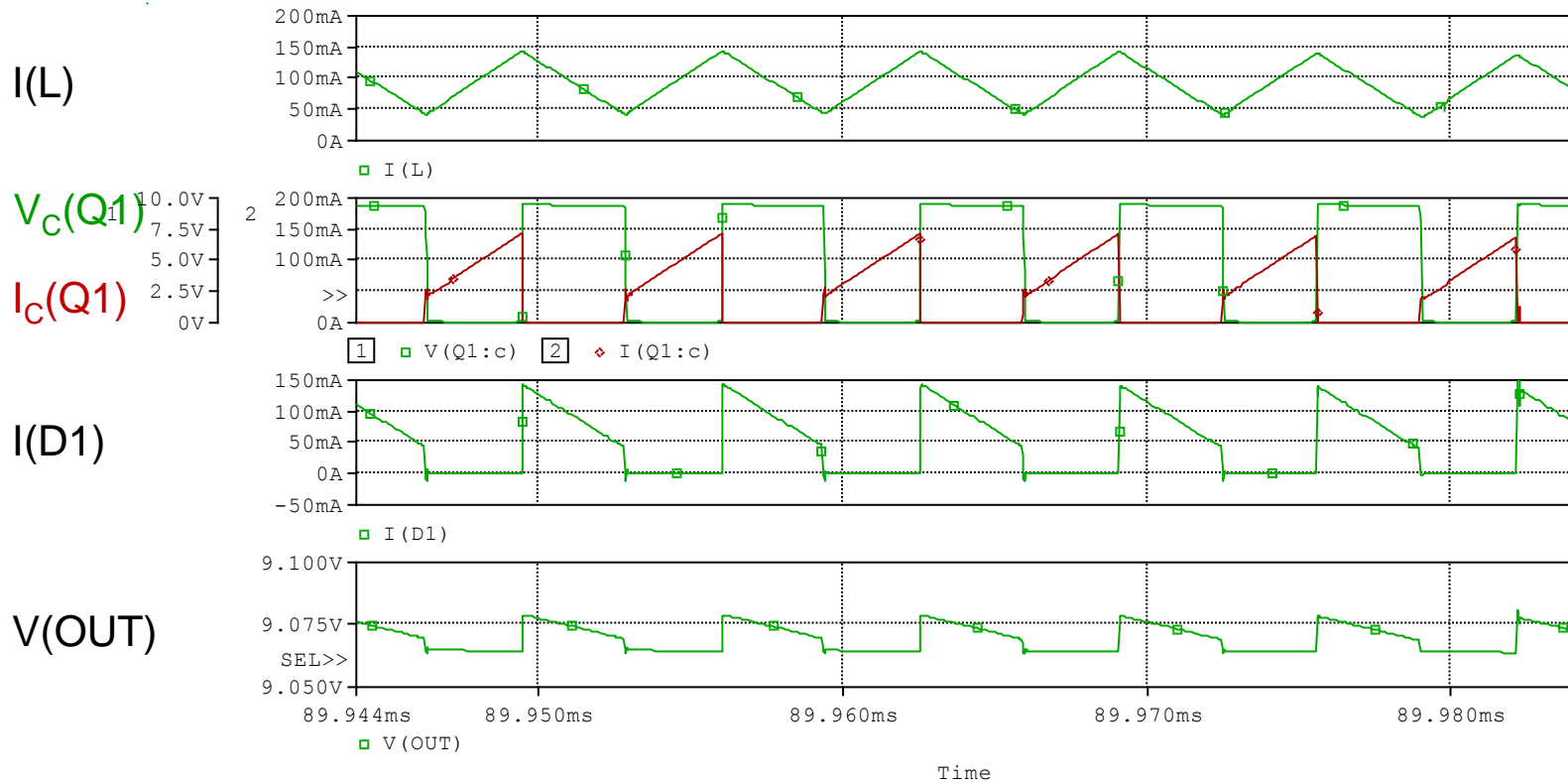
- Simulation result shows waveforms of I_F and V_{AK} of diode D1. Loss in peak and average values are also shown.

7.1 Start-Up Sequencing Waveforms



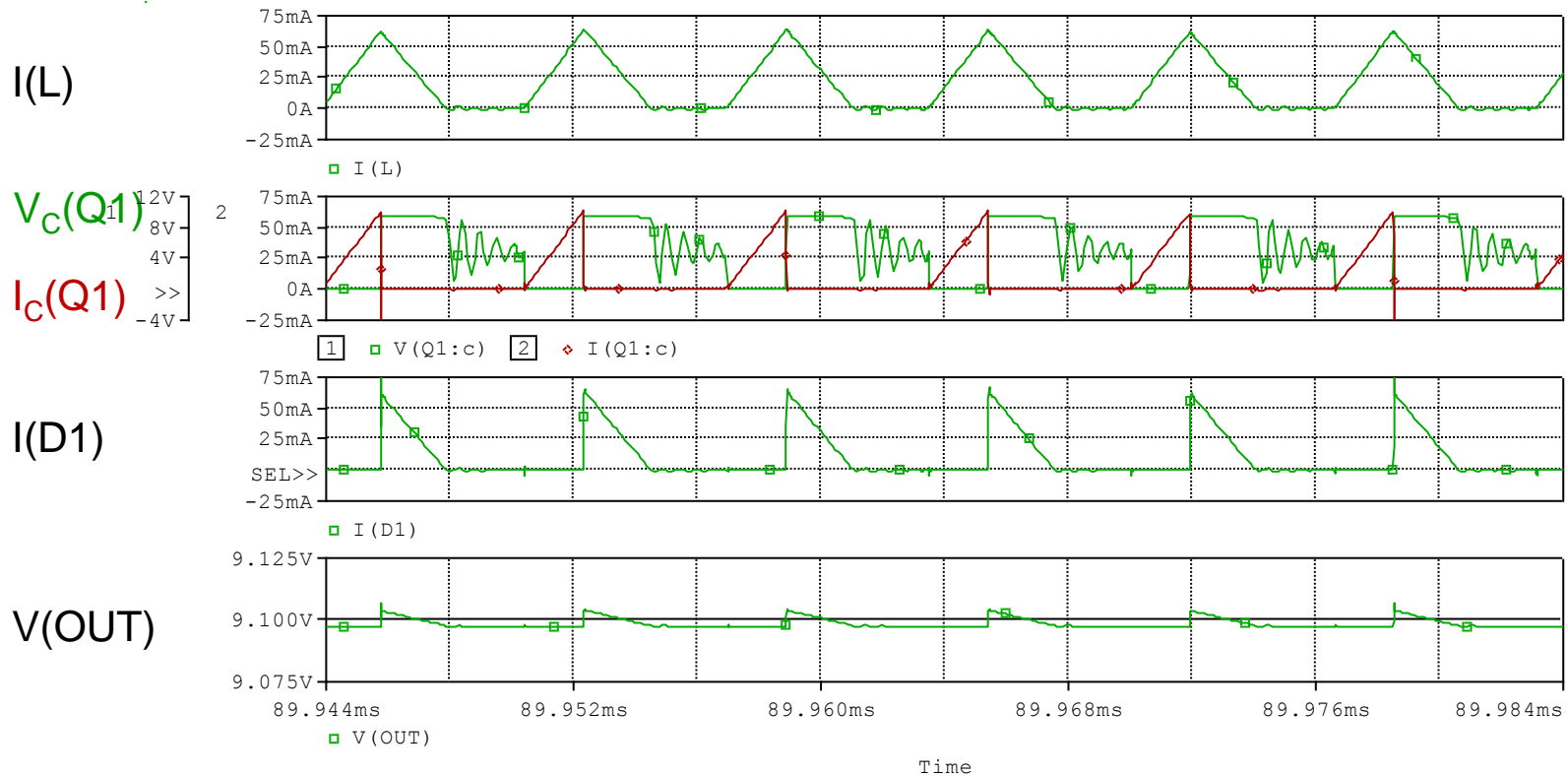
- Simulation result shows start-up sequencing waveforms, including $V(OUT)$ and control signal (V_{RAMP} , V_{OSC} , and V_{FB}).

7.2 Switching Waveforms at Load 50 mA ($R_L=180\Omega$)



- Simulation result shows boost converter switching waveforms at load 50mA, including I_L , $V_C(Q1)$, $I_C(Q1)$, $I(D1)$ and $V(OUT)$

7.3 Switching Waveforms at Load 10 mA ($R_L=900\Omega$)



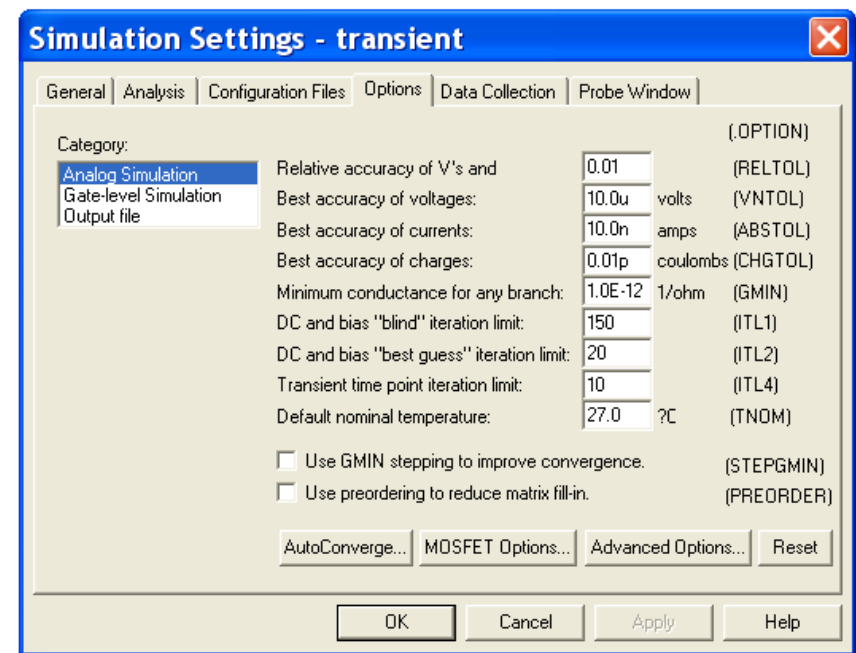
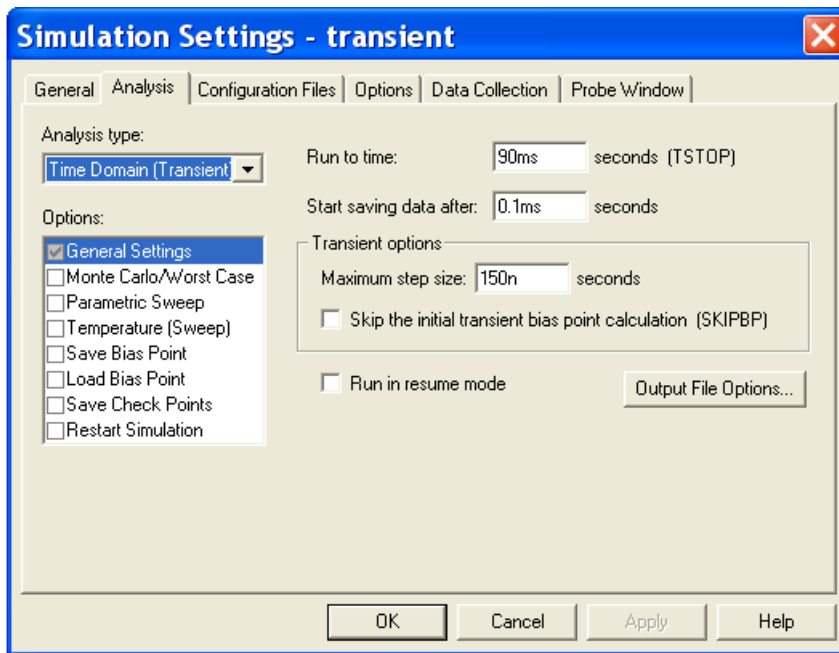
- Simulation result shows boost converter switching waveforms at load 10mA, including I_L , $V_C(Q1)$, $I_C(Q1)$, $I(D1)$ and $V(OUT)$

Simulations	Page	Folder name
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2. NJM2377 – Oscillation Frequency Setting.....	13	\IC-Config\OSC
3. Error Amp Feed Back Loop (Transient).....	14	\IC-Config\FB
4. Start-Up Transient Simulation (0~90ms.).....	16, 17, 23	Transient
5. Efficiency and Losses.....	18, 21, 22	Efficiency
6. Step-Load Response.....	19	Step-load
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8. Switching Waveforms.....	8, 9, 24, 25	Waveforms

SIMULATION SETTINGS 1

These settings are for:

- Start-Up Transient Simulation (0~90ms.)
- Voltage and Current Simulation
- Step-Load Response

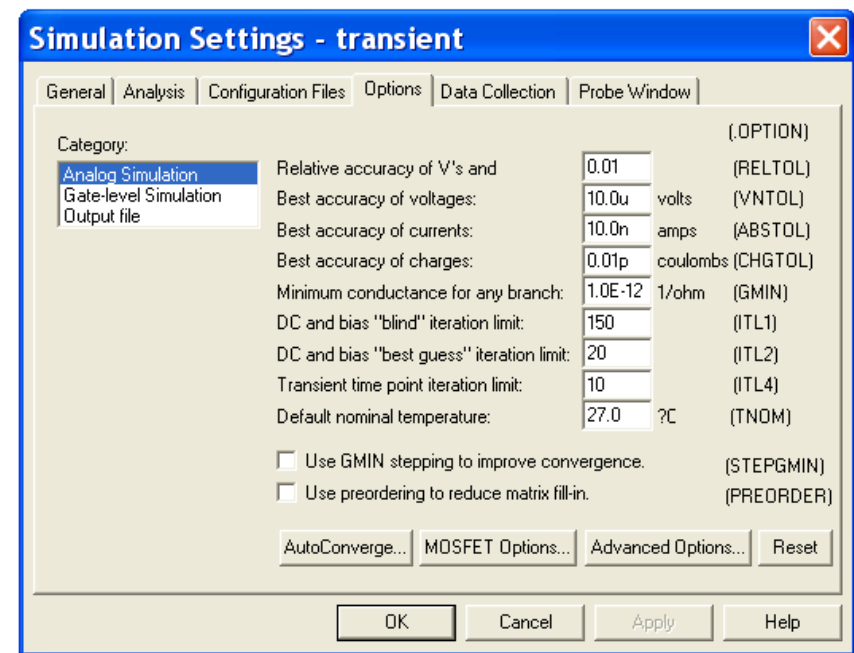
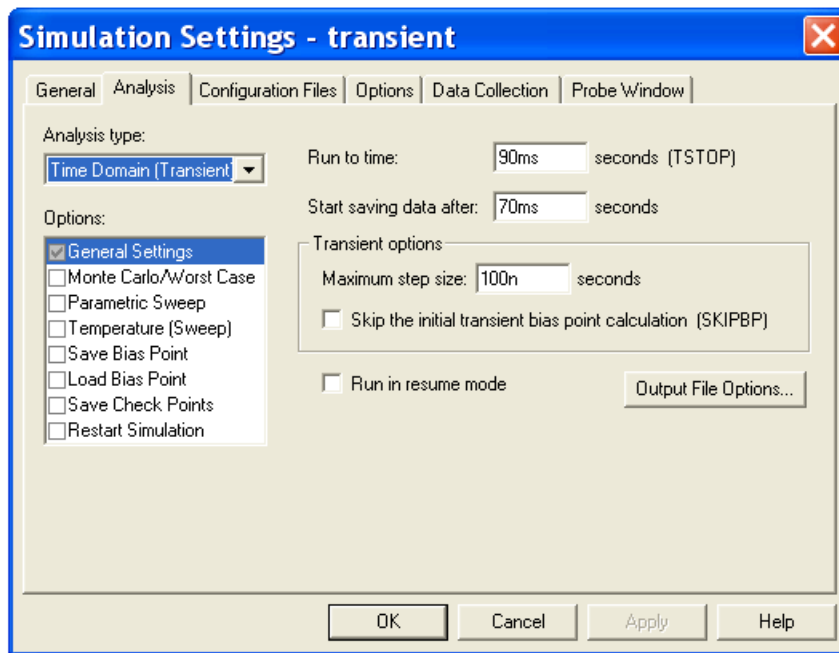


- .TRAN 0 90ms 0.1ms 150n
- .OPTIONS ABSTOL= 10.0n
- .OPTIONS RELTOL= 0.01
- .OPTIONS VNTOL= 10.0u

SIMULATION SETTINGS 2

These settings are for:

- Efficiency and Losses
- Switching Waveforms



- .TRAN 0 90ms 70ms 100n
- .OPTIONS ABSTOL= 10.0n
- .OPTIONS RELTOL= 0.01
- .OPTIONS VNTOL= 10.0u